



RP

Oil Pump and Motor Sets

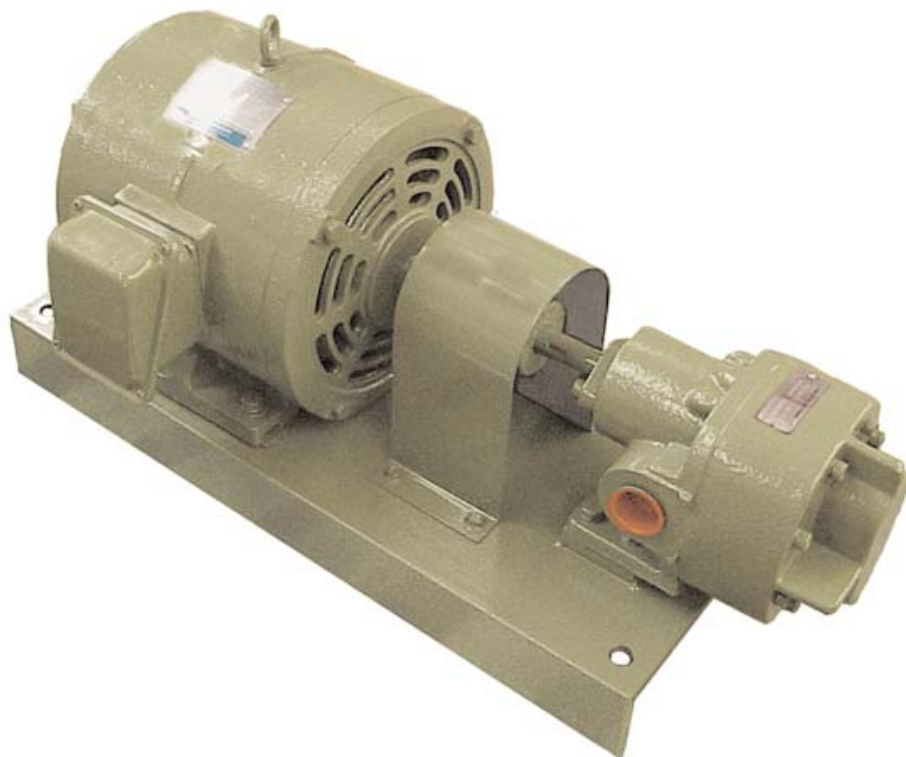


Features

- Available with ODP or TEFC motors
- Factory assembled
- Capacities to 3200 gph

Benefits

- Quiet operation
- Long service life



Hauck's RP series pump and motor sets are factory assembled units designed to meet your specific volume, viscosity, and discharge pressure requirements. Each set combines a positive displacement rotary gear pump with a suitable 'T' frame industrial electric motor mounted on a steel base. The motor and pump are matched to ensure that the requirements of the application are met with maximum efficiency.

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Combustion Excellence Since 1888

RP-1



Hauck Manufacturing Company

RP

OIL PUMP AND MOTOR SETS



ADVANTAGES OF THE RP

Factory Assembled

Quiet Operation

Long Service Life

Construction

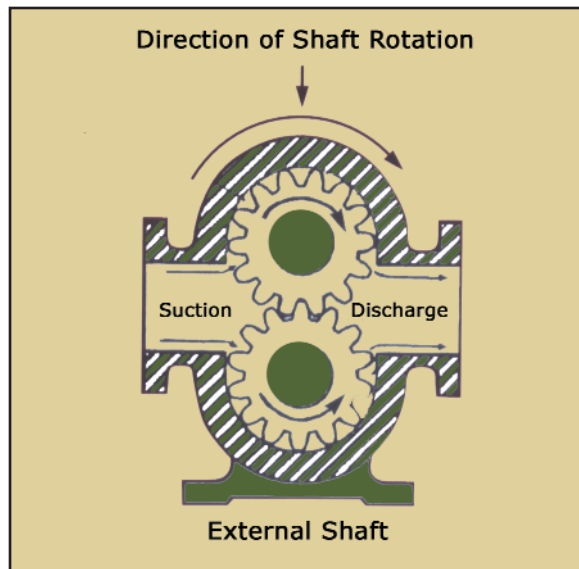
RP pump units consist of a pump, motor, direct coupling, and shaft and coupling guard (as required by OSHA standards) - all preassembled and mounted on a steel base.

The pump's helical herringbone gears are fabricated of high-alloy steel to provide quiet, pulse-free flow and prevent the trapping of liquids. All internal bearings are force-fed lubricated by the liquid passing through the pump. The drive shafts are made from hardened steel and ground to meet high quality control standards.

The electric motors are furnished by leading industrial motor manufacturers who maintain stringent inspection procedures to ensure long service life. The motors are available in two models; open, drip proof (ODP) and totally enclosed, fan cooled (TEFC).

Operation

The specific operational characteristics of each assembly will depend on the pump and motor selected. However, a pressure relief valve must be installed immediately downstream of the pump. This pressure relief valve (bypass valve) should be designed and adjusted to control and maintain the required pump discharge pressure of either 50, 100, or 150 psig.



Schematic representation of the pump showing the oil flow path.

Required Suction Head

A characteristic of each pump, determined by test or computation, is the required N.P.S.H (net positive suction head). It is the maximum amount of suction pressure* the pump can develop without cavitation to pull the oil into the pump. In other words, it is the maximum amount of suction pressure available to lift the oil, if required, and overcome pressure losses in the inlet piping to the pump.

The required N.P.S.H. varies with the pump design and pump size. The values listed in the table below refer to the pump sizes listed in the RP-2 (Capacities) product literature.

* In absolute pressure

Required N.P.S.H

| PUMP SIZE | VISCOSITY | | | | | |
|--------------|-----------|-----------|------------|-------------|-------------|---------------|
| | 40 SSU | 90 SSU | 400 SSU | 2000 SSU | 3000 SSU | 10,000 SSU |
| 1 | 6.3 | 6.5 | 6.8 | 7.5 | 7.8 | 8.8 |
| 2 | 6.5 | 6.8 | 7.3 | 8.0 | 8.0 | 9.5 |
| 3 | 7.5 | 7.8 | 9.0 | 10.0 | 10.3 | 12.0 |
| 4 | 7.5 | 7.8 | 9.0 | 10.0 | 10.3 | 12.0 |
| 5 | 8.5 | 8.8 | 9.5 | 10.8 | 11.5 | 15.0 |
| 6 | 8.5 | 8.8 | 9.5 | 10.8 | 11.5 | 15.0 |



CAPACITIES

RP OIL PUMP AND MOTOR SETS

SELECTION TABLES*

| TABLE 1 40 SSU -- VISCOSITY | | | |
|--------------------------------|--------------------|-----------------------------|--------------------|
| 50 PSIG DISCHARGE PRESSURE | | 100 PSIG DISCHARGE PRESSURE | |
| GPH | MODEL NO. | GPH | MODEL NO. |
| 132 | RP1-56-1/2-1200 | 102 | RP1-56-1/2-1200 |
| 204 | RP1-56-1/2-1800 | 168 | RP2-143-3/4-1200 |
| 240 | RP2-56-1/2-1200 | 174 | RP1-56-1/2-1800 |
| 384 | RP2-56-1/2-1800 | 336 | RP2-143-1-1800 |
| 582 | RP3-143-3/4-1200 | 450 | RP3-182-1 1/2-1200 |
| 828 | RP4-145-1-1200 | 756 | RP4-184-2-1200 |
| 948 | RP3-145-1 1/2-1800 | 840 | RP3-145-2-1800 |
| 1272 | RP5-184-2-1200 | 1020 | RP5-213-3-1200 |
| 1416 | RP4-145-1 1/2-1800 | 1302 | RP4-182-3-1800 |
| 1920 | RP6-184-2-1200 | 1680 | RP6-213-3-1200 |
| 2100 | RP5-182-3-1800 | 1920 | RP5-184-5-1800 |
| 3060 | RP6-184-5-1800 | 2808 | RP6-184-5-1800 |

| TABLE 2 90 SSU -- VISCOSITY | | | |
|--------------------------------|--------------------|-----------------------------|--------------------|
| 50 PSIG DISCHARGE PRESSURE | | 100 PSIG DISCHARGE PRESSURE | |
| GPH | MODEL NO. | GPH | MODEL NO. |
| 168 | RP1-56-1/2-1200 | 138 | RP1-56-1/2-1200 |
| 252 | RP1-56-1/2-1800 | 222 | RP1-56-1/2-1800 |
| 354 | RP2-56-1/2-1200 | 330 | RP2-143-3/4-1200 |
| 528 | RP2-56-1/2-1800 | 504 | RP2-143-1-1800 |
| 636 | RP3-143-3/4-1200 | 570 | RP3-145-1-1200 |
| 918 | RP4-145-1-1200 | 846 | RP4-182-1 1/2-1200 |
| 996 | RP3-145-1 1/2-1800 | 930 | RP3-145-2-1800 |
| 1416 | RP5-184-2-1200 | 1266 | RP3-213-3-1200 |
| 1512 | RP4-145-2-1800 | 1428 | RP4-182-3-1800 |
| 2010 | RP6-213-3-1200 | 1812 | RP6-215-5-1200 |
| 2220 | RP5-182-3-1800 | 2088 | RP5-184-5-1800 |
| 3192 | RP6-184-5-1800 | 2988 | RP6-213-7 1/2-1800 |

| TABLE 3 2000 SSU -- VISCOSITY | | | | | |
|----------------------------------|--------------------|-----------------------------|--------------------|-----------------------------|--------------------|
| 50 PSIG DISCHARGE PRESSURE | | 100 PSIG DISCHARGE PRESSURE | | 150 PSIG DISCHARGE PRESSURE | |
| GPH | MODEL NO. | GPH | MODEL NO. | GPH | MODEL NO. |
| 174 | RP1-56-1/2-1200 | 162 | RP1-56-1/2-1200 | 150 | RP1-56-1/2-1200 |
| 276 | RP1-56-1/2-1800 | 258 | RP1-56-1/2-1800 | 240 | RP1-56-3/4-1800 |
| 360 | RP2-56-1/2-1200 | 348 | RP2-143-3/4-1200 | 336 | RP2-145-1-1200 |
| 588 | RP2-143-1-1800 | 576 | RP2-145-1 1/2-1800 | 552 | RP2-145-1 1/2-1800 |
| 678 | RP3-145-1-1200 | 660 | RP3-182-1 1/2-1200 | 648 | RP3-184-2-1200 |
| 1050 | RP4-182-1 1/2-1200 | 1020 | RP4-184-2-1200 | 960 | RP4-213-3-1200 |
| 1050 | RP3-145-2-1800 | 1020 | RP3-182-3-1800 | 966 | RP3-145-3-1800 |
| 1500 | RP5-213-3-1200 | 1422 | RP5-215-5-1200 | 1350 | RP5-215-5-1200 |
| 1620 | RP4-182-3-1800 | 1572 | RP4-184-5-1800 | 1530 | RP4-184-5-1800 |
| 2172 | RP6-215-5-1200 | 2052 | RP6-215-5-1200 | 1980 | RP6-254-7 1/2-1200 |
| 2322 | RP5-184-5-1800 | 2250 | RP5-213-7 1/2-1800 | 2172 | RP5-213-7 1/2-1800 |
| 3270 | RP6-213-7 1/2-1800 | 3180 | RP6-213-7 1/2-1800 | 3090 | RP6-215-10-1800 |

*All calculations are based on a 60 Hertz motor of 1200 or 1800 RPM. Horsepowers shown reflect recommended motor sizes and not actual horsepower consumed. Detailed pump/motor graphs are available on request.

SELECTION

The proper selection of a pump and motor assembly requires the consideration of many factors. Chief among these are:

1. desired discharge pressure
2. required peak capacity, and
3. the viscosity of the oil to be pumped.

The final factor, the most important from a selection point of view, is often misunderstood or completely overlooked. It is a common misconception that "temperature" can be substituted for viscosity. To see why this is not the case, viscosity will be discussed in some detail.

The viscosity of a fluid is a measure of its internal resistance to flow. Seconds, Saybolt Universal (SSU) is a commonly used measure of viscosity. Using this scale, viscosity is expressed in terms of the number of seconds required for a specific amount of oil to flow through an orifice; hence, the larger the number in seconds (SSU), the higher the viscosity. The higher the viscosity, the more the oil approaches the solid state. The lower the viscosity, the more easily the oil flows. The viscosity of an oil can be altered by heating. Viscosity decreases with increases in temperature. When heavy oils are used, it is necessary to reduce the viscosity of the oil by raising the oil temperature.

(OVER)

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When heating oil, *even of the same grade*, widely varying viscosities are obtained at the same temperature. For example, heating No. 6 oil to 125° will yield a viscosity in the range of 650 to 1250 SSU. This means that two samples of No. 6 oil (in two different deliveries for example) can vary in viscosity, at 125°, by 600 SSU – or more. Obviously, stating the grade of oil and its temperature is not enough to determine the viscosity, and viscosity is critical to the proper selection of a pump assembly. A viscometer or other suitable device should be used to determine the viscosity of the oil at the pump suction opening.

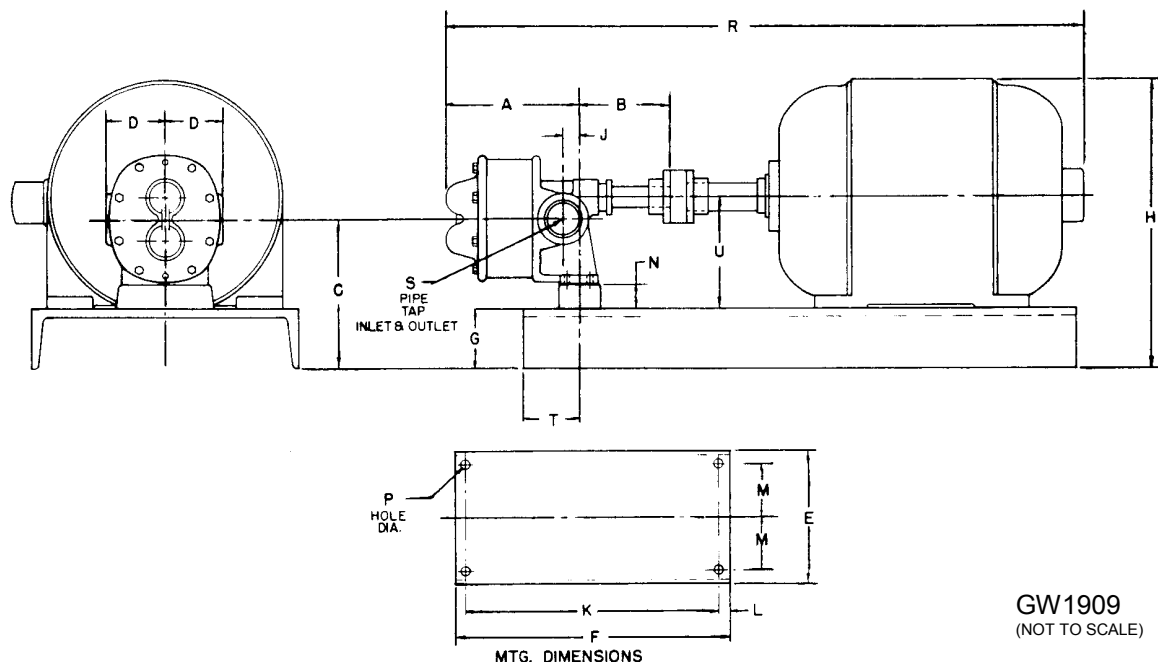
If oil temperature at the pump is expected to exceed 200°F, a high temperature seal is recommended. Please specify this requirement at time of ordering.

The SELECTION TABLES on the previous page offer pump assemblies having a wide range of flow capacities, discharge pressures, and viscosity-handling capabilities. Tables 1-3 present various combinations of these 3 elements and the model number associated with each combination. If the table entries do not cover your particular application requirements, or if additional information is needed, detailed graphs of each pump are available upon request. Consult your local Hauck representative.



DIMENSIONS

RP OIL PUMP AND MOTOR SETS



| MODEL NO. | RP1-56 | RP1-143 | RP2-56 | RP2-143 | RP2-145 | RP2-182 | RP3-143 8.4-143 | RP3-145 8.4-145 | RP3-182 8.4-182 | RP3-184 8.4-184 | RP3-213 8.4-213 | RP3-215 8.4-215 | RP5-182 8.6-182 | RP5-184 8.6-184 | RP5-213 8.6-213 | RP5-215 8.6-215 | RP5-254 8.6-254 | RP5-256 8.6-256 |
|-------------|--------------------|--------------------|-------------------|--------------------|--------------------|--------------------|----------------------|--------------------|--------------------|--------------------|--------------------|--------------------|----------------------|--------------------|--------------------|--------------------|--------------------|--------------------|
| SIZE PUMP | 1-GA. | | 2-GA. | | | | 3 & 4-GA. (SEE NOTE) | | | | | | 5 & 6-GA. (SEE NOTE) | | | | | |
| MOTOR FRAME | K56 | 143T | 56 | 143T | 145T | 182T | 143T | 145T | 182T | 184T | 213T | 215T | 182T | 184T | 213T | 215T | 254T | 256T |
| A | 3 $\frac{7}{8}$ | 3 $\frac{7}{8}$ | 4 $\frac{11}{16}$ | 4 $\frac{11}{16}$ | 4 $\frac{11}{16}$ | 4 $\frac{11}{16}$ | 6 | 6 | 6 | 6 | 6 | 6 | 7 $\frac{1}{2}$ | 7 $\frac{1}{2}$ | 7 $\frac{1}{2}$ | 7 $\frac{1}{2}$ | 7 $\frac{1}{2}$ | 7 $\frac{1}{2}$ |
| B | 3 $\frac{1}{4}$ | 3 $\frac{1}{4}$ | 3 $\frac{3}{4}$ | 3 $\frac{3}{4}$ | 3 $\frac{3}{4}$ | 3 $\frac{3}{4}$ | 4 $\frac{1}{2}$ | | | | | | 5 $\frac{1}{8}$ | | | | | |
| C | 5 $\frac{5}{16}$ | 5 $\frac{5}{16}$ | 5 $\frac{7}{32}$ | 5 $\frac{7}{32}$ | 5 $\frac{7}{32}$ | 6 $\frac{19}{32}$ | 5 $\frac{1}{2}$ | 5 $\frac{1}{2}$ | 6 $\frac{1}{4}$ | 6 $\frac{1}{4}$ | 7 $\frac{3}{8}$ | 7 $\frac{3}{8}$ | 6 $\frac{3}{16}$ | 6 $\frac{3}{16}$ | 7 $\frac{3}{16}$ | 7 $\frac{3}{16}$ | 8 $\frac{11}{16}$ | 8 $\frac{11}{16}$ |
| D | 1 $\frac{5}{8}$ | 1 $\frac{5}{8}$ | 2 $\frac{1}{8}$ | | | | 2 $\frac{1}{4}$ | | | | | | 3 $\frac{1}{4}$ | | | | | |
| E | 8 | 8 | 8 | 8 | 8 | 10 | 10 | 10 | 10 | 10 | 12 | 12 | 10 | 10 | 12 | 12 | 15 | 15 |
| F | 19 $\frac{1}{2}$ | 19 $\frac{1}{2}$ | 19 $\frac{1}{2}$ | 19 $\frac{1}{2}$ | 19 $\frac{1}{2}$ | 23 | 23 | 23 | 23 | 23 | 26 | 26 | 23 | 23 | 26 | 26 | 31 | 31 |
| G | 2 $\frac{1}{4}$ | | | | | 2 $\frac{5}{8}$ | 2 $\frac{5}{8}$ | 2 $\frac{5}{8}$ | 2 $\frac{5}{8}$ | 2 $\frac{5}{8}$ | 3 | 3 | 2 $\frac{5}{8}$ | 2 $\frac{5}{8}$ | 3 | 3 | 3 $\frac{3}{8}$ | 3 $\frac{3}{8}$ |
| H | 9 $\frac{1}{8}$ | 9 $\frac{1}{8}$ | 9 $\frac{1}{8}$ | 9 $\frac{1}{8}$ | 9 $\frac{1}{8}$ | 12 $\frac{1}{16}$ | 9 $\frac{3}{4}$ | 9 $\frac{3}{4}$ | 11 $\frac{1}{16}$ | 11 $\frac{1}{16}$ | 13 $\frac{7}{8}$ | 13 $\frac{7}{8}$ | 12 $\frac{1}{16}$ | 12 $\frac{1}{16}$ | 13 $\frac{7}{8}$ | 13 $\frac{7}{8}$ | 16 $\frac{7}{16}$ | 16 $\frac{7}{16}$ |
| H* | 9 $\frac{9}{16}$ | 9 $\frac{9}{16}$ | 9 $\frac{9}{16}$ | 9 $\frac{9}{16}$ | 9 $\frac{9}{16}$ | 12 $\frac{3}{8}$ | 10 | 10 | 12 $\frac{1}{4}$ | 12 $\frac{1}{4}$ | 14 | 14 | 12 $\frac{3}{8}$ | 12 $\frac{3}{8}$ | 14 | 14 | 16 $\frac{17}{32}$ | 16 $\frac{17}{32}$ |
| J | 1 $\frac{11}{16}$ | 1 $\frac{11}{16}$ | 2 | | | | 1 | | | | | | 7 $\frac{7}{8}$ | | | | | |
| K | 17 $\frac{3}{4}$ | 17 $\frac{3}{4}$ | | | | 21 $\frac{1}{4}$ | 21 $\frac{1}{4}$ | 21 $\frac{1}{4}$ | 21 $\frac{1}{4}$ | 21 $\frac{1}{4}$ | 23 $\frac{1}{2}$ | 23 $\frac{1}{2}$ | 21 $\frac{1}{4}$ | 21 $\frac{1}{4}$ | 23 $\frac{1}{2}$ | 23 $\frac{1}{2}$ | 28 $\frac{1}{2}$ | 28 $\frac{1}{2}$ |
| L | 7 $\frac{7}{8}$ | 7 $\frac{7}{8}$ | | | | 7 $\frac{7}{8}$ | 7 $\frac{7}{8}$ | 7 $\frac{7}{8}$ | 7 $\frac{7}{8}$ | 7 $\frac{7}{8}$ | 1 $\frac{1}{4}$ | 1 $\frac{1}{4}$ | 7 $\frac{7}{8}$ | 7 $\frac{7}{8}$ | 1 $\frac{1}{4}$ | 1 $\frac{1}{4}$ | 1 $\frac{1}{4}$ | 1 $\frac{1}{4}$ |
| M | 3 | 3 | 3 | 3 | 3 | 4 | 4 | 4 | 4 | 4 | 4 $\frac{3}{4}$ | 4 $\frac{3}{4}$ | 4 | 4 | 4 $\frac{3}{4}$ | 4 $\frac{3}{4}$ | 6 | 6 |
| N | 1 $\frac{1}{4}$ | 1 $\frac{1}{4}$ | 5 $\frac{5}{8}$ | 5 $\frac{5}{8}$ | 5 $\frac{5}{8}$ | 5 $\frac{5}{8}$ | 0 | 0 | 3 $\frac{1}{4}$ | 3 $\frac{1}{4}$ | 1 $\frac{1}{2}$ | 1 $\frac{1}{2}$ | 0 | 0 | 5 $\frac{5}{8}$ | 5 $\frac{5}{8}$ | 1 $\frac{3}{4}$ | 1 $\frac{3}{4}$ |
| P | 5 $\frac{5}{8}$ | 5 $\frac{5}{8}$ | 5 $\frac{5}{8}$ | 5 $\frac{5}{8}$ | 5 $\frac{5}{8}$ | 5 $\frac{5}{8}$ | 5 $\frac{5}{8}$ | 5 $\frac{5}{8}$ | 5 $\frac{5}{8}$ | 5 $\frac{5}{8}$ | 1 | 1 | 5 $\frac{5}{8}$ | 5 $\frac{5}{8}$ | 1 | 1 | 1 | 1 |
| R | 16 $\frac{11}{16}$ | 20 $\frac{5}{16}$ | 19 $\frac{1}{8}$ | 21 $\frac{5}{8}$ | 21 $\frac{5}{8}$ | 21 $\frac{11}{16}$ | 23 $\frac{11}{16}$ | 23 $\frac{11}{16}$ | 23 $\frac{3}{4}$ | 25 $\frac{1}{8}$ | 27 | 28 $\frac{1}{2}$ | 25 $\frac{7}{8}$ | 27 $\frac{1}{4}$ | 29 $\frac{1}{8}$ | 30 $\frac{5}{8}$ | 34 | 35 $\frac{3}{4}$ |
| R* | 18 $\frac{1}{16}$ | 20 $\frac{21}{32}$ | 19 $\frac{5}{16}$ | 21 $\frac{31}{32}$ | 21 $\frac{31}{32}$ | 23 $\frac{1}{4}$ | 24 $\frac{1}{32}$ | 24 $\frac{1}{32}$ | 25 $\frac{5}{16}$ | 26 $\frac{1}{16}$ | 29 | 30 $\frac{1}{2}$ | 27 $\frac{7}{16}$ | 28 $\frac{13}{16}$ | 31 $\frac{1}{8}$ | 32 $\frac{5}{8}$ | 36 $\frac{5}{16}$ | 38 $\frac{1}{16}$ |
| S | 1 $\frac{1}{2}$ | 1 $\frac{1}{2}$ | 3 $\frac{3}{4}$ | 3 $\frac{3}{4}$ | 3 $\frac{3}{4}$ | 3 $\frac{3}{4}$ | 1 | | | | | | 1 $\frac{1}{2}$ | | | | | |
| T | 1 $\frac{7}{8}$ | 1 $\frac{7}{8}$ | 2 $\frac{7}{8}$ | 2 $\frac{7}{8}$ | 2 $\frac{7}{8}$ | 2 $\frac{7}{8}$ | 2 $\frac{7}{8}$ | 2 $\frac{7}{8}$ | 2 $\frac{7}{8}$ | 2 $\frac{7}{8}$ | 3 $\frac{1}{4}$ | 3 $\frac{1}{4}$ | 2 $\frac{7}{8}$ | 2 $\frac{7}{8}$ | 2 $\frac{7}{8}$ | 2 $\frac{7}{8}$ | 2 $\frac{7}{8}$ | 2 $\frac{7}{8}$ |
| U | 3 $\frac{5}{8}$ | 3 $\frac{5}{8}$ | 3 $\frac{5}{8}$ | 3 $\frac{5}{8}$ | 3 $\frac{5}{8}$ | 4 $\frac{5}{8}$ | 3 $\frac{7}{8}$ | 3 $\frac{7}{8}$ | 4 $\frac{5}{8}$ | 4 $\frac{5}{8}$ | 5 $\frac{3}{8}$ | 5 $\frac{3}{8}$ | 4 $\frac{3}{4}$ | 4 $\frac{3}{4}$ | 5 $\frac{3}{8}$ | 5 $\frac{3}{8}$ | 6 $\frac{1}{2}$ | 6 $\frac{1}{2}$ |

NOTE: 3 GA. DIM. A & R" LESS $\frac{5}{8}$ "
 5 GA. DIM. A & R" LESS $\frac{3}{4}$ " * TEFC

GX1909
(NOT TO SCALE)

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